### FEATURES
- LESS THAN ±1% TOTAL ADJUSTED ERROR, –40°C TO +85°C
- RTD EXCITATION AND LINEARIZATION
- TWO OR THREE-WIRE RTD OPERATION
- WIDE SUPPLY RANGE: 9V to 40V
- HIGH PSR: 110dB min
- HIGH CMR: 80dB min

### APPLICATIONS
- INDUSTRIAL PROCESS CONTROL
- FACTORY AUTOMATION
- SCADA

#### DESCRIPTION
The XTR103 is a monolithic 4-20mA, two-wire current transmitter designed for Platinum RTD temperature sensors. It provides complete RTD current excitation, instrumentation amplifier, linearization, and current output circuitry on a single integrated circuit. Versatile linearization circuitry provides a 2nd-order correction to the RTD, typically achieving a 40:1 improvement in linearity.

Instrumentation amplifier gain can be configured for a wide range of temperature measurements. Total adjusted error of the complete current transmitter, including the linearized RTD is less than ±1% over the full –40 to +85°C operating temperature range. This includes zero drift, span drift and nonlinearity. The XTR103 operates on loop power supply voltages down to 9V.

The XTR103 is available in 16-pin plastic DIP and SOL-16 surface-mount packages specified for the –40°C to +85°C temperature range.
**SPECIFICATIONS**

**ELECTRICAL**

At $T_A = +25^\circ C$, $V_+ = 24V$, and 2N6121 external transistor, unless otherwise noted.

### OUTPUT

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Output Current Equation</td>
<td></td>
<td>MIN</td>
<td>TYP</td>
<td>MAX</td>
</tr>
<tr>
<td>Total Adjusted Error</td>
<td>$T_{MIN}$ to $T_{MAX}$</td>
<td>20%</td>
<td>±2%</td>
<td>% of FS</td>
</tr>
<tr>
<td>Output Current, Specified Range</td>
<td>$I_0 = V_{IN} \cdot (0.016 + 40/R_G)$</td>
<td>4mA</td>
<td>0.016mA</td>
<td>0.016mA</td>
</tr>
<tr>
<td>Over-Scale Limit</td>
<td></td>
<td>34%</td>
<td>40%</td>
<td>mA</td>
</tr>
<tr>
<td>Under Scale-Limit</td>
<td></td>
<td>3.6%</td>
<td>3.8%</td>
<td>mA</td>
</tr>
<tr>
<td>Full Scale Output Error</td>
<td>$V_{IN} = 1V$, $R_G = \infty$</td>
<td>±15</td>
<td>±50</td>
<td>μA</td>
</tr>
</tbody>
</table>
| Noise: 0.1Hz to 1kHz                   |                  | 8           | *           | μA/ap-

### ZER0 OUTPUT

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Initial Error</td>
<td>$V_{IN} = 0$, $R_G = \infty$</td>
<td>4 mA</td>
<td>*</td>
<td>mA</td>
</tr>
<tr>
<td>vs Temperature</td>
<td></td>
<td>±5</td>
<td>+5</td>
<td>mA/V</td>
</tr>
<tr>
<td>vs Supply Voltage, $V_+$</td>
<td></td>
<td>±0.2</td>
<td>±0.5</td>
<td>μA/C</td>
</tr>
<tr>
<td>vs Common-Mode Voltage</td>
<td>$V_{CM} = 2V$ to $4V$</td>
<td>0.1</td>
<td>2</td>
<td>μA/V</td>
</tr>
</tbody>
</table>

### SPAN

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Span Equation (Transconductance)</td>
<td></td>
<td>S = $0.016 + 40/R_G$</td>
<td>*</td>
<td>A/V</td>
</tr>
<tr>
<td>Untrimmed Error</td>
<td></td>
<td>$R_G \geq 75\Omega$</td>
<td>±0.1</td>
<td>%</td>
</tr>
<tr>
<td>vs Temperature</td>
<td>$R_G \geq 75\Omega$</td>
<td>±20</td>
<td>±50</td>
<td>%</td>
</tr>
<tr>
<td>Nonlinearity: Ideal Input</td>
<td></td>
<td>0.01</td>
<td>*</td>
<td>%</td>
</tr>
<tr>
<td>RTD Input</td>
<td>$R_{LIN} = 1127\Omega$</td>
<td>0.1</td>
<td>*</td>
<td>%</td>
</tr>
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### INPUT

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
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</thead>
<tbody>
<tr>
<td>Differential Range</td>
<td>$R_G = \infty$</td>
<td>2</td>
<td>1</td>
<td>V</td>
</tr>
<tr>
<td>Input Voltage Range</td>
<td></td>
<td>4</td>
<td>4</td>
<td>V</td>
</tr>
<tr>
<td>Common-Mode Rejection</td>
<td>$V_{IN} = 2V$ to $4V$</td>
<td>30</td>
<td>100</td>
<td>dB</td>
</tr>
<tr>
<td>Impedance: Differential</td>
<td>3</td>
<td>*</td>
<td>*</td>
<td>GO</td>
</tr>
<tr>
<td>Common-Mode</td>
<td>0.5</td>
<td>*</td>
<td>GΩ</td>
<td></td>
</tr>
<tr>
<td>Offset Voltage</td>
<td></td>
<td>±0.5</td>
<td>±2.5</td>
<td>mV</td>
</tr>
<tr>
<td>vs Temperature</td>
<td></td>
<td>±1</td>
<td>±2.5</td>
<td>μV/C</td>
</tr>
<tr>
<td>vs Supply Voltage, $V_+$</td>
<td>$V_+ = 9V$ to $40V$</td>
<td>110</td>
<td>130</td>
<td>dB</td>
</tr>
<tr>
<td>Input Bias Current</td>
<td>100</td>
<td>*</td>
<td>*</td>
<td>nA</td>
</tr>
<tr>
<td>vs Temperature</td>
<td></td>
<td>2</td>
<td>2</td>
<td>nA</td>
</tr>
<tr>
<td>Input Offset Current</td>
<td></td>
<td>0.1</td>
<td>0.25</td>
<td>nA/C</td>
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</tbody>
</table>

### CURRENT SOURCES

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
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<th>UNITS</th>
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<tbody>
<tr>
<td>Current</td>
<td></td>
<td>0.8</td>
<td>*</td>
<td>mA</td>
</tr>
<tr>
<td>Accuracy</td>
<td></td>
<td>±0.25</td>
<td>±0.5</td>
<td>%</td>
</tr>
<tr>
<td>vs Temperature</td>
<td>$V_+ = 9V$ to $40V$</td>
<td>50</td>
<td>*</td>
<td>ppm/V</td>
</tr>
<tr>
<td>Compliance Voltage</td>
<td></td>
<td>*</td>
<td>*</td>
<td>V</td>
</tr>
<tr>
<td>Matching</td>
<td>$V_{IN} = 0$</td>
<td>±0.5</td>
<td>*</td>
<td>%</td>
</tr>
<tr>
<td>vs Temperature</td>
<td>$V_+ = 9V$ to $40V$</td>
<td>10</td>
<td>*</td>
<td>ppm/V</td>
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</table>

### POWER SUPPLY

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
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</thead>
<tbody>
<tr>
<td>Voltage Range</td>
<td>$V_+$</td>
<td>9</td>
<td>40</td>
<td>V</td>
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### TEMPERATURE RANGE

<table>
<thead>
<tr>
<th>PARAMETER</th>
<th>CONDITIONS</th>
<th>XTR103BP/BU</th>
<th>XTR103AP/AU</th>
<th>UNITS</th>
</tr>
</thead>
<tbody>
<tr>
<td>Specification, $T_{MIN}$ to $T_{MAX}$</td>
<td></td>
<td>−40</td>
<td>85</td>
<td>°C</td>
</tr>
<tr>
<td>Operating</td>
<td></td>
<td>−40</td>
<td>125</td>
<td>°C</td>
</tr>
<tr>
<td>$\theta_{JA}$</td>
<td></td>
<td>80</td>
<td>*</td>
<td>°C/W</td>
</tr>
</tbody>
</table>

* Specification same as XTR103BP.

**NOTES:** (1) Includes corrected Pt100 nonlinearity for process measurement spans greater than 100°C, and over-temperature zero and span effects. Does not include initial offset and gain errors which are normally trimmed to zero at 25°C. (2) Describes accuracy of the 4mA low-scale offset current. Does not include input amplifier effects. Can be trimmed to zero. (3) Voltage measured with respect to $I_0$ pin. (4) Does not include TCR of gain-setting resistor, $R_G$. (5) Measured with $R_{LIN} = \infty$ to disable linearization feature.
PIN CONFIGURATION

TOP VIEW

<table>
<thead>
<tr>
<th>1</th>
<th>Zero Adjust</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>3</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>4</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>5</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>6</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>7</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>8</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>9</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>10</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>11</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>12</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>13</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>14</td>
<td>Zero Adjust</td>
</tr>
<tr>
<td>15</td>
<td>Zero Adjust</td>
</tr>
</tbody>
</table>

ABSOLUTE MAXIMUM RATINGS

- Power Supply, V+ (referenced to IO pin) .......................................... 40V
- Input Voltage, V+IN, V–IN (referenced to IO pin) ........................ 0V to V+
- Storage Temperature Range ........................................ –55°C to +125°C
- Lead Temperature (soldering, 10s) .............................................. +300°C
- Output Current Limit ............................................................... Continuous
- Junction Temperature ............................................................... +165°C

ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Burr-Brown recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

<table>
<thead>
<tr>
<th>PRODUCT</th>
<th>PACKAGE</th>
<th>PACKAGE DRAWING NUMBER</th>
<th>TEMPERATURE RANGE</th>
</tr>
</thead>
<tbody>
<tr>
<td>XTR103AP</td>
<td>16-pin Plastic DIP</td>
<td>180</td>
<td>–40°C to +85°C</td>
</tr>
<tr>
<td>XTR103BP</td>
<td>16-pin Plastic DIP</td>
<td>180</td>
<td>–40°C to +85°C</td>
</tr>
<tr>
<td>XTR103AU</td>
<td>SOL-16 Surface Mount</td>
<td>211</td>
<td>–40°C to +85°C</td>
</tr>
<tr>
<td>XTR103BU</td>
<td>SOL-16 Surface Mount</td>
<td>211</td>
<td>–40°C to +85°C</td>
</tr>
</tbody>
</table>

NOTE: (1) For detailed drawing and dimension table, please see end of data sheet, or Appendix C of Burr-Brown IC Data Book.

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TYPICAL PERFORMANCE CURVES

At $T_A = +25^\circ C$, $V_+ = 24VDC$, unless otherwise noted.
TYPICAL PERFORMANCE CURVES (CONT)

At $T_A = +25^\circ C$, $+V = 24VDC$, unless otherwise noted.

OUTPUT CURRENT NOISE DENSITY vs FREQUENCY

Input Current Noise (pA/Hz)

0.1 1 100 1k 100k

Frequency (Hz)

INPUT CURRENT NOISE DENSITY vs FREQUENCY

0.1 1 100 1k 100k

Frequency (Hz)

INPUT VOLTAGE NOISE DENSITY vs FREQUENCY

Noise Voltage (nV/Hz)

10 100 1k 10k 100k

Frequency (Hz)
APPLICATION INFORMATION

Figure 1 shows the basic connection diagram for the XTR103. The loop power supply, \( V_{PS} \), provides power for all circuitry. Output loop current is measured as a voltage across the series load resistor, \( R_L \).

Two matched 0.8mA current sources drive the RTD and zero-setting resistor, \( R_Z \). The instrumentation amplifier input of the XTR103 measures the voltage difference between the RTD and \( R_Z \). The value of \( R_Z \) is chosen to be equal to the resistance of the RTD at the low-scale (minimum) measurement temperature. \( R_G \) can be adjusted to achieve 4mA output at the minimum measurement temperature to correct for input offset voltage and reference current mismatch of the XTR103.

\( R_{CM} \) provides an additional voltage drop to bias the inputs of the XTR103 within their common-mode range. Resistor, \( R_G \), sets the gain of the instrumentation amplifier according to the desired temperature measurement range.

The transfer function through the complete instrumentation amplifier and voltage-to-current converter is:

\[
I_O = V_{IN} \cdot (0.016 + 40/R_G) + 4mA,
\]

\( (V_{IN} \text{ in volts, } R_G \text{ in ohms, } R_{LIN} = \infty) \)

where \( V_{IN} \) is the differential input voltage. With no \( R_G \) connected (\( R_G = \infty \)), a 0V to 1V input produces a 4-20mA output current. With \( R_G = 25 \Omega \), a 0V to 10mV input produces a 4-20mA output current. Other values for \( R_G \) can be calculated according to the desired full-scale input voltage, \( V_{FS} \), with the formula in Figure 1.

Negative input voltage, \( V_{IN} \), will cause the output current to be less than 4mA. Increasingly negative \( V_{IN} \) will cause the output current to limit at approximately 3.6mA.

Increasingly positive input voltage (greater than \( V_{FS} \)) will produce increasing output current according to the transfer function, up to the output current limit of approximately 34mA.

EXTERNAL TRANSISTOR

Transistor \( Q_1 \) conducts the majority of the signal-dependent 4-20mA loop current. Using an external transistor isolates the majority of the power dissipation from the precision input and reference circuitry of the XTR103, maintaining excellent accuracy.

Since the external transistor is inside a feedback loop its characteristics are not critical. Requirements are: \( V_{CEO} = 45V \text{ min, } \beta = 40 \text{ min and } P_D = 800mW \). Power dissipation requirements may be lower if the loop power supply voltage is less than 40V. Some possible choices for \( Q_1 \) are listed in Figure 1.

The XTR103 can be operated without this external transistor by connecting pin 11 to 14 (see Figure 2). Accuracy will be somewhat degraded by the additional internal power dissipation. This effect is most pronounced when the input stage is set for high gain (for low full-scale input voltage). The typical performance curve “Input Offset Voltage vs Loop Supply Voltage” describes this behavior.

![FIGURE 1. Basic RTD Temperature Measurement Circuit.](image-url)
The low operating voltage (9V) of the XTR103 allows operation directly from personal computer power supplies (12V ±5%). When used with the RCV420 Current Loop Receiver (Figure 8), load resistor voltage drop is limited to 1.5V.

**LINEARIZATION**

On-chip linearization circuitry creates a signal-dependent variation in the two matching current sources. Both current sources are varied equally according to the following equation:

\[
I_{R1} = I_{R2} = 0.8 + \frac{500 \cdot V_{IN}}{R_{LIN}}
\]

\(I_R\) in mA, \(V_{IN}\) in volts, \(R_{LIN}\) in ohms

(maximum \(I_R\) = 1.0mA)

This varying excitation provides a 2nd-order term to the transfer function (including the RTD) which can correct the RTD’s nonlinearity. The correction is controlled by resistor \(R_{LIN}\) which is chosen according to the desired temperature measurement range. Table I provides the \(R_G\), \(R_Z\) and \(R_{LIN}\) resistor values for a Pt100 RTD.

If no linearity correction is desired, do not connect a resistor to the \(R_{LIN}\) pins (\(R_{LIN} = \infty\)). This will cause the excitation current sources to remain a constant 0.8mA.

**ADJUSTING INITIAL ERRORS**

Most applications will require adjustment of initial errors. Offset errors can be corrected by adjustment of the zero resistor, \(R_Z\).

Figure 3 shows another way to adjust zero errors using the output current adjustment pins of the XTR103. This provides a minimum of ±300µA (typically ±500µA) adjustment around the initial low-scale output current. This is an output current adjustment which is independent of the input stage gain set.
with \( R_G \). If the input stage is set for high gain (as required with narrow temperature measurement spans) the output current adjustment may not provide sufficient range. In these cases, offset can be nulled by adjusting the value of \( R_Z \).

**TWO-WIRE AND THREE-WIRE RTD CONNECTIONS**

In Figure 1, the RTD can be located remotely simply by extending the two connections to the RTD. With this two-wire connection to the RTD, line resistance will introduce error. This error can be partially corrected by adjusting the values of \( R_Z, R_G \), and \( R_{LIN} \).

**OPEN-CIRCUIT DETECTION**

The optional transistor \( Q_2 \) in Figure 4 provides predictable behavior with open-circuit RTD connections. It assures that if any one of the three RTD connections is broken, the XTR103’s output current will go to either its high current limit (≈34mA) or low current limit (≈3.6mA). This is easily detected as an out-of-range condition.

**REVERSE-VOLTAGE PROTECTION**

Figure 5 shows two ways to protect against reversed output connection lines. Trade-offs in an application will determine which technique is better. \( D_1 \) offers series protection, but causes a 0.7V loss in loop supply voltage. This may be undesirable if \( V+ \) can approach the 9V limit. Using \( D_2 \) (without \( D_1 \)) has no voltage loss, but high current will flow in the loop supply if the leads are reversed. This could damage the power supply or the sense resistor, \( R_L \). A diode with a higher current rating is needed for \( D_2 \) to withstand the highest current that could occur with reversed lines.

**SURGE PROTECTION**

Long lines are subject to voltage surges which can damage semiconductor components. To avoid damage, the maximum applied voltage rating for the XTR103 is 40V. A zener diode may be used for \( D_2 \) (Figure 6) to clamp the voltage applied to the XTR103 to a safe level. The loop power supply voltage must be lower than the voltage rating of the zener diode.
There are special zener diode types specifically designed to provide a very low impedance clamp and withstand large energy surges. These devices normally have a diode characteristic in the forward direction which also protects against reversed loop connections. As noted earlier, reversed loop connections would produce a large loop current, possibly damaging $R_L$.

**RADIO FREQUENCY INTERFERENCE**

The long wire lengths of current loops invite radio frequency interference. RF can be rectified by the sensitive input circuitry of the XTR103 causing errors. This generally appears as an unstable output current that varies with the position of loop supply or input wiring.

If the RTD sensor is remotely located, the interference may enter at the input terminals. For integrated transmitter assemblies with short connection to the sensor, the interference more likely comes from the current loop connections. Bypass capacitors on the input often reduce or eliminate this interference. Connect these bypass capacitors to the $I_O$ terminal as shown in Figure 7. Although the DC voltage at the $I_O$ terminal is not equal to 0V (at the loop supply, $V_{PS}$) this circuit point can be considered the transmitter’s “ground.”

---

**FIGURE 5. Reverse Voltage Protection.**

**FIGURE 6. Over-Voltage Surge Protection.**
FIGURE 7. Input Bypassing Techniques.

FIGURE 8. ±12V-Powered Transmitter/Receiver Loop.

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